

# Radar Backscatter Measurement Accuracies Using Digital Doppler Processors in Spaceborne Scatterometers

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**Abstract**—The normalized standard deviation,  $K_p$ , of radar backscatter measurements using digital Doppler processors in spaceborne scatterometers is derived. The  $K_p$  expression for analog Doppler filter processors, such as that used in the Seasat scatterometer [7] is shown to be a special case of the derived  $K_p$  expression. A connection to Welch's power spectrum estimation results [6] is also made. Tradeoff studies in digital filter design such as hardware complexity, computational speed, and system performance can be performed based on this  $K_p$  expression. We briefly discuss a current application in the design of the NASA scatterometer (NSCAT) to be flown in 1990. This derivation should be useful for system design and analysis of other radar remote-sensing instruments.

## I. INTRODUCTION

A SCATTEROMETER is a radar system that measures the normalized scattering coefficient  $\sigma_0$  of an illuminated surface by measuring the return signal power of a radar backscatter signal [1]. Scatterometers have been flown on the spaceborne platforms Skylab and Seasat. The Seasat scatterometer (SASS) demonstrated the ability to infer wind speed and direction over the ocean from  $\sigma_0$  measurements [2], [3]. Using the radar equation and the measured return signal power  $P_r$ ,  $\sigma_0$  can be computed using the well-known radar equation

$$\sigma_0 = \frac{(4\pi)^3 R^4 P_r}{P_t G^2 \lambda^2 A L} \quad (1)$$

where

- $P_t$  is the transmitted signal power;
- $G$  is the antenna gain;
- $\lambda$  is the wavelength of the signal;
- $A$  is the Doppler cell area;
- $R$  is the slant range to the illuminated Doppler cell; and
- $L$  is the system loss.

SASS used four dual-polarized (vertical and horizontal polarizations) fan-beam antennas pointed at  $45^\circ$  and  $135^\circ$  relative to the spacecraft flight direction to produce an X-shaped illumination pattern on the Earth. In this way a

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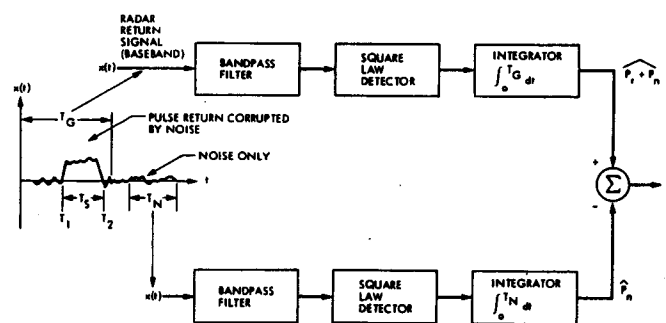


Fig. 1. Signal processing system for a scatterometer using analog filters.

given surface location was first viewed by a forward-looking antenna, and then viewed by an aft-looking antenna some time later. A train of microwave pulses was transmitted to the Earth's surface. The reflected signal for each pulse was Doppler shifted due to relative motion of the spaceborne scatterometer with respect to the Earth's surface. Signals from different locations in the antenna illumination pattern will have different Doppler shifts, and, by separating the return signal in the Doppler spectral domain, the desired along-beam resolution can be achieved. We will refer to each of the Doppler-shifted resolution cells as a " $\sigma_0$  cell."

SASS utilized analog devices for signal power estimates. These consisted of bandpass filters, square-law detectors, and gated integrators (see Fig. 1). The fixed frequency bands used in the bandpass filters caused radar system performance degradation in several areas. The Doppler shifts induced by the Earth's rotation caused the locations of the  $\sigma_0$  cells of the forward-looking antenna beams to shift relative to those of the aft looking beams. This led to a loss in swath coverage as well as misregistration of the  $\sigma_0$  cells. The misregistration could produce errors in the inferred wind vectors when wind gradients are present. A solution to these problems is to use a digital signal processor in which the frequency bands of the  $\sigma_0$  cells can be adjusted to compensate for the Earth's rotation.

Such a digital processor is planned for use on the NASA scatterometer (NSCAT) to be flown in 1990 [4], [5]. The fast Fourier transform (FFT)-based digital processor allows the Doppler frequencies of  $\sigma_0$  cells to be adjusted in order to maintain nearly constant cross-track distances

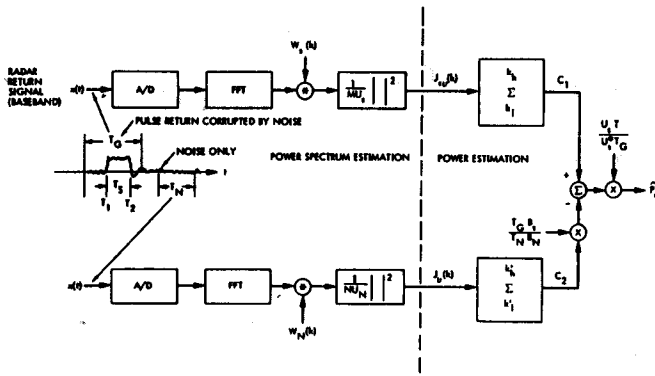


Fig. 2. Signal processing system for a scatterometer using FFT-based digital processing.

from the spacecraft ground track for the  $\sigma_0$  cells. An additional advantage of the FFT-based digital processing scheme is that the Doppler center frequency and bandwidth of the  $\sigma_0$  cells can be readily modified to compensate for slight variations in orbital parameters due to launch errors or in-orbit maneuvers.

A schematic diagram of the NSCAT digital processing technique is shown in Fig. 2. The scatterometer return signal is passed through the top path to estimate the power  $C_1$  of the signal plus noise. A separate measurement is made using the bottom path to estimate the noise power,  $C_2$  alone. Both of these measurements are telemetered to ground for further processing. In the ground data processing, an unbiased estimate of the backscatter power  $P_r$  is obtained by a linear combination of  $C_1$  and  $C_2$ .

Each path in Fig. 2 consists of the following on-board instrument functions: a) computation of the FFT, b) application of a window by convolution, c) squaring for power detection, and d) computation of the signal power within a  $\sigma_0$  cell by summing the result of c) over the frequency bins corresponding to the range of Doppler frequencies of that  $\sigma_0$  cell. In effect, a), b), and c) provide Welch's power spectrum estimates [6] of the scatterometer return signal, and d) acts as a bandpass filter. During ground processing the unbiased estimate of  $P_r$  is then used to determine the radar backscatter cross section  $\sigma_0$ .

Data windowing is used in step b) to reduce spectral leakage. This reduces any bias in the estimated signal power caused by "interference" between  $\sigma_0$  cells. This interference can be severe in situations where there are large variations in the power spectrum of the return signal, such as in the case of a strong wind gradient over the ocean. Although the variance of Welch's spectrum estimate has little dependence on the window itself, the variance of the power estimate over a frequency band may increase due to correlation between frequency bins caused by windowing. Thus, windowing may adversely affect the accuracy of the signal power estimate. In order to minimize this degradation in the power estimate accuracy, temporal-domain overlapped processing of the FFT data segments is used in step c).

A commonly adopted parameter for evaluating the performance of spaceborne scatterometers is the so-called  $K_p$

parameter [7]. It is defined to be the normalized standard deviation of the measured  $\sigma_0$ ,  $\hat{\sigma}_0$ , i.e.

$$K_p = \frac{\{\text{Var}[\hat{\sigma}_0]\}^{1/2}}{\sigma_0} \quad (2)$$

where  $\text{Var}[\hat{\sigma}_0]$  is the variance of  $\hat{\sigma}_0$ . The smaller the value of  $K_p$ , the better the estimate of  $\sigma_0$  is. A general goal in scatterometer design is to minimize  $K_p$ .

The  $K_p$  equation for an analog signal power estimator, such as that used on SASS, was derived by Fisher [7]. In this paper, we derive the  $K_p$  equation for the digital signal processor shown in Fig. 2. The derived expression for  $K_p$ , which is more complicated than that for the analog case, is being used to make processor design and performance tradeoffs for NSCAT. We feel that this derivation should be useful for system design and analysis of other radar remote sensing instruments.

In Section II, we briefly review Welch's power spectrum estimation. The expression for  $K_p$  is then derived in detail in Section III. Two illustrative examples are described in Section IV. Finally, we briefly discuss the utility of this equation in scatterometer system design in Section V.

## II. MEAN AND COVARIANCE OF WELCH'S POWER SPECTRUM ESTIMATION FOR STATIONARY GAUSSIAN PROCESSES

In subsequent analysis, we will frequently use the mean and covariance of Welch's power spectral estimation for stationary Gaussian processes. The expressions for mean and variance can be found in [6]. The covariance, however, is not commonly found in the literature. In this section, we briefly describe the expression for the covariance. Details of the derivation are shown in Appendix I.

Let  $x(n)$ ,  $n = 0, 1, 2, \dots, L-1$  be the given real data set sampled from a zero-mean stationary Gaussian random process with power spectral density (psd)  $P_x(\omega)$ . Segments of these sampled data, possibly overlapping, of length  $M$  with starting points of the segments  $D$  units apart are constructed. Assuming that we have  $K$  such segments  $x_i(n)$ ,  $i = 1, 2, \dots, K$  that cover the entire record. Then  $x_i(n)$  is given by

$$x_i(n) = \begin{cases} x(n + (i-1)D), & 0 \leq n \leq M-1 \\ 0, & \text{otherwise} \end{cases} \quad (3)$$

with  $(K-1)D + M = L$ . The modified periodogram for each segment is defined as [6], [8]

$$\begin{aligned} J_i(\omega) &= \frac{1}{MU_i} \left| \sum_{n=0}^{M-1} x_i(n) \gamma_i(n) e^{-j\omega n} \right|^2 \\ &= \frac{1}{MU_i} |X_i(\omega) * \Gamma_i(\omega)|^2 \end{aligned} \quad (4)$$

where  $X_i(\omega)$  and  $\Gamma_i(\omega)$  are the Fourier transform of  $x_i(n)$  and the data window  $\gamma_i(n)$ , respectively, and

$$U_i = \frac{1}{M} \sum_{n=0}^{M-1} \gamma_i^2(n). \quad (5)$$

The Welch's power spectrum estimate,  $J(\omega)$ , is defined as [6], [8]

$$J(\omega) = \frac{1}{K} \sum_{i=1}^K J_i(\omega). \quad (6)$$

Let us assume that the bandwidths of the windows  $\gamma_i(n)$  and  $\gamma_{ij}(n)$  are narrow compared to the variations of the power spectrum  $P_x(\omega)$  where

$$\gamma_{ij}(n) = \gamma_i(n) \gamma_j(n + (i - j) D). \quad (7)$$

Finally, we assume that

$$|\Gamma_{ij}(\omega_1 - \omega_2)|^2 \gg |\Gamma_{ij}(\omega_1 + \omega_2)|^2, \quad (8)$$

for all  $\omega_1, \omega_2 \in (\omega_a, \omega_b)$ .

(Note that the value of  $P_x(\omega)$  outside  $(\omega_a, \omega_b)$  is not needed in the following discussion.)

Assuming that  $P_x(\omega)$  is constant over the frequency band  $(\omega_a, \omega_b)$ , i.e.

$$P_x(\omega) = P, \quad \text{for all } \omega \in (\omega_a, \omega_b) \quad (9)$$

then one can easily show that [6], [8]

$$\begin{aligned} E[J(\omega)] &= E[J_i(\omega)] \\ &= \frac{1}{MU_i} \frac{1}{2\pi} \int_{-\pi}^{\pi} P_x(\theta) |\Gamma_i(\omega - \theta)|^2 d\theta \\ &= \left(\frac{1}{MU_i}\right) \left(\frac{1}{2\pi}\right) P \\ &\quad \int_{-\pi}^{\pi} |\Gamma_i(\omega - \theta)|^2 d\theta = P \quad \forall \omega \in (\omega_a, \omega_b). \end{aligned} \quad (10)$$

The autocovariance function of  $J(\omega)$ , as derived in Appendix I, is given by

$$\begin{aligned} \text{Cov} \{J(\omega_1), J(\omega_2)\} \\ &= \frac{1}{K^2} \frac{P^2}{M^2} \sum_{i=1}^K \sum_{j=1}^K \left(\frac{1}{U_i U_j}\right) |\Gamma_{ij}(\omega_1 - \omega_2)|^2 \\ &\quad \forall \omega_1, \omega_2 \in (\omega_a, \omega_b). \end{aligned} \quad (11)$$

### III. DERIVATION OF $K_p$

From (1) and (2),  $K_p$  can be expressed as

$$K_p = \frac{\{\text{Var} [\hat{P}_r]\}^{1/2}}{P_r} \quad (12)$$

where  $\hat{P}_r$  is the output of the signal power estimator in Fig. 2 and  $\text{Var} [\hat{P}_r]$  is its variance.

From Fig. 2, one can see that the scatterometer received signal  $x(t)$  can be modeled as

$$x(t) = s(t) \text{rect}(t - T_1) + \nu(t) \quad (13) \quad \text{where}$$

where

$$\text{rect}(t) = \begin{cases} 1, & 0 < t < T_s \\ 0, & \text{otherwise} \end{cases} \quad (14) \quad \text{with}$$

$s(t)$  is the returned signal,  $T_1$  and  $T_s$  are the starting time and the pulse length of the received signal, respectively, and  $\nu(t)$  is noise. We assume that the scatterometer signal from the Earth's surface can be modeled as a stationary bandlimited Gaussian process (see [1]).

$$P_s(f) = 0, \quad \text{for } |f| > f_s/2 \quad (15)$$

where  $f_s$  is the Nyquist sampling frequency. The noise  $\nu(t)$  is assumed to be a stationary Gaussian process with zero mean and power spectral density

$$P_\nu(f) = b, \quad \text{for } |f| < f_s/2 \quad (16)$$

i.e.,  $P_\nu(f)$  is constant over all the frequency range. Furthermore, we assume that

$$P_s(f) = P_r/B_s, \quad \text{for } f_l \leq f \leq f_h = f_l + B_s, \quad (17)$$

where  $P_r$  is the power of  $s(t)$  over the frequency range  $(f_l, f_h)$  and  $B_s$  is the bandwidth used for a given  $\sigma_0$  cell. Thus, the psd's for  $s(n)$  and  $\nu(n)$  are

$$P_\nu(\omega) = \frac{b}{T}, \quad 0 \leq \omega < 2\pi \quad (18)$$

$$P_s(\omega) = \frac{P_r}{B_s T}, \quad \omega_l \leq \omega \leq \omega_h \quad (19)$$

where  $\omega_h = 2\pi f_h T$ ,  $\omega_l = 2\pi f_l T$  and  $T = 1/f_s$ .

The derivation of the  $K_p$  expression for the system shown in Fig. 2 is performed in three steps. First, the mean and variance of the output  $C_1$  of the top path in Fig. 2 are derived. Second, the mean and variance of the output  $C_2$  of the bottom path in Fig. 2 are derived. Finally, the unbiased estimate  $\hat{P}_r$  of  $P_r$ , obtained by a linear combination of  $C_1$  and  $C_2$ , and its normalized standard deviation,  $K_p$ , are derived. These steps are shown in the following subsections.

We assume that the number of data segments, the number of data points in each segment and the window function are  $K_1$ ,  $M$ , and  $w_s(n)$  for the top path and  $K_2$ ,  $N$ , and  $w_N(n)$  for the bottom path in Fig. 2. We also assume that  $D = D_1$  and  $D = D_2$  for the top and bottom paths, respectively. First, we concentrate on the mean and variance of  $C_1$ .

#### A. Mean and Variance of $C_1$

Welch's spectrum estimate for the top (signal plus noise) path in Fig. 2 that contains  $K_1$  data segment overlapping  $M$ - $D$  points is given by

$$J_{sv}(\omega) = \frac{1}{K_1} \sum_{i=1}^{K_1} J_{sv_i}(\omega) \quad (20)$$

$$J_{sv_i}(\omega) = \frac{1}{MU_s} \left| \sum_{n=0}^{M-1} x_i(n) w_s(n) e^{-j\omega n} \right|^2 \quad (21)$$

$$U_s = \frac{1}{M} \sum_{n=0}^{M-1} w_s^2(n). \quad (22)$$

where

$$U_s^* = \frac{1}{K_1} \sum_{i=1}^{K_1} U_i. \quad (35)$$

We can express  $x_i(n) w_s(n)$  as (see (13))

$$x_i(n) w_s(n) = x_{s_i}(n) + x_{v_i}(n) \quad (23)$$

where

$$x_{v_i}(n) = v_i(n) w_s(n) = v_i(n + (i-1)D_1) w_s(n) \quad (24)$$

$$x_{s_i}(n) = s(n + (i-1)D_1) \gamma_i(n) \quad (25)$$

with

$$\gamma_i(n) = \begin{cases} \text{rect}(nT + (i-1)D_1T - T_1) w_s(n), & 0 \leq n \leq M-1 \\ 0, & \text{otherwise.} \end{cases} \quad (26)$$

From (21) and (23) we have

$$J_{sv}(\omega) = \left(\frac{U_i}{U_s}\right) J_{s_i}(\omega) + J_{v_i}(\omega) + \frac{1}{MU_s} [X_{s_i}(\omega) X_{v_i}^*(\omega) + X_{s_i}^*(\omega) X_{v_i}(\omega)] \quad (27)$$

where

$$J_{s_i}(\omega) = \left(\frac{1}{MU_i}\right) \left| \sum_{n=0}^{M-1} x_{s_i}(n) e^{-j\omega n} \right|^2 = \left(\frac{1}{MU_i}\right) |X_{s_i}(\omega)|^2 \quad (28)$$

and

$$J_{v_i}(\omega) = \left(\frac{1}{MU_s}\right) \left| \sum_{n=0}^{M-1} x_{v_i}(n) e^{-j\omega n} \right|^2 = \frac{1}{MU_s} |X_{v_i}(\omega)|^2. \quad (29)$$

From (20) and (27) we get

$$J_{sv}(\omega) = J_s(\omega) + J_v(\omega) + I_{sv}(\omega) \quad (30)$$

where

$$J_s(\omega) = \frac{1}{U_s K_1} \sum_{i=1}^{K_1} U_i J_{s_i}(\omega) \quad (31)$$

$$J_v(\omega) = \frac{1}{K_1} \sum_{i=1}^{K_1} J_{v_i}(\omega) \quad (32)$$

and

$$I_{sv}(\omega) = \frac{1}{MU_s} \frac{1}{K_1} \sum_{i=1}^{K_1} [X_{s_i}(\omega) X_{v_i}^*(\omega) + X_{s_i}^*(\omega) X_{v_i}(\omega)]. \quad (33)$$

From (10), (18), (19), (30), (31), (32), and (33) we have

$$\begin{aligned} E[J_{sv}(\omega)] &= \frac{1}{U_s K_1} \sum_{i=1}^{K_1} U_i \left(\frac{P_r}{B_s T}\right) + \frac{1}{K_1} \sum_{i=1}^{K_1} \left(\frac{b}{T}\right) \\ &= \frac{U_s^*}{U_s} \left(\frac{P_r}{B_s T}\right) + \frac{b}{T}, \quad \text{for } \omega \in (\omega_l, \omega_h) \end{aligned} \quad (34)$$

We note that  $E[I_{sv}(\omega)] = 0$  because  $E[X_{s_i}(\omega) X_{v_i}^*(\omega)] = E[X_{s_i}(\omega)] E[X_{v_i}^*(\omega)] = 0$ , and similarly,  $E[X_{s_i}^*(\omega) X_{v_i}(\omega)] = 0$ .

Since

$$C_1 = \sum_{k=k_l}^{k_h} J_{sv}(k) \quad (36)$$

where  $k_l$  and  $k_h$  are the smallest and largest integers in  $(f_l MT, f_h MT)$ , respectively, and  $J_{sv}(k) = J_{sv}(\omega = 2\pi k/M)$ , the mean value of  $C_1$  is

$$\begin{aligned} E[C_1] &= k_s \left(\frac{U_s^* P_r}{U_s B_s T} + \frac{b}{T}\right) \\ &= M \left(\frac{f_h - f_l}{f_s}\right) \left(\frac{U_s^* P_r}{U_s B_s T} + \frac{b}{T}\right) \\ &= \frac{T_G B_s}{T} \left(\frac{U_s^* P_r}{U_s B_s} + b\right) \end{aligned} \quad (37)$$

where  $k_s = (k_h - k_l + 1) \cong T_G B_s$  and  $T_G = MT$ . Notice that  $T_G B_s$  is not necessarily an integer. Therefore, there must be a roundoff error between  $T_G B_s$  and  $k_s$ . In this paper, we neglect this minor issue.

From (30), we also have

$$\begin{aligned} \text{Cov}\{J_{sv}(\omega_1), J_{sv}(\omega_2)\} &= \text{Cov}\{J_s(\omega_1), J_s(\omega_2)\} \\ &\quad + \text{Cov}\{J_v(\omega_1), J_v(\omega_2)\} \\ &\quad + \text{Cov}\{I_{sv}(\omega_1), I_{sv}(\omega_2)\} \end{aligned} \quad (38)$$

because  $J_s(\omega)$ ,  $J_v(\omega)$ , and  $I_{sv}(\omega)$  are mutually uncorrelated. From (11), the first and second terms of (38) can be written as

$$\begin{aligned} \text{Cov}\{J_s(\omega_1), J_s(\omega_2)\} &= \left(\frac{P_r}{K_1 U_s T_G B_s}\right)^2 \\ &\quad \cdot \sum_{i=1}^{K_1} \sum_{j=1}^{K_1} |\Gamma_{ij}(\omega_1 - \omega_2)|^2 \\ &\quad \omega_1, \omega_2 \in (\omega_l, \omega_h) \end{aligned} \quad (39)$$

and

$$\begin{aligned} \text{Cov}\{J_v(\omega_1), J_v(\omega_2)\} &= \left(\frac{b}{K_1 U_s T_G}\right)^2 \\ &\quad \cdot \sum_{i=1}^{K_1} \sum_{j=1}^{K_1} |W_s(i-j, \omega_1 - \omega_2)|^2 \\ &\quad \omega_1, \omega_2 \in (\omega_l, \omega_h) \end{aligned} \quad (40)$$

where  $W_s(q, \omega)$  is the Fourier transform of

$$w_s(q, n) = w_s(n) w_s(n + qD_1). \quad (41)$$

The third term of (38) is given by (see Appendix III)

$$\begin{aligned} \text{Cov} \{I_{sv}(\omega_1), I_{sv}(\omega_2)\} &\equiv \left(\frac{P_r}{B_s}\right) b \left(\frac{1}{T_G U_s K_1}\right)^2 \\ &\sum_{i=1}^{K_1} \sum_{j=1}^{K_1} \{ \Gamma_{ij}(\omega_1 - \omega_2) W_s^*(i - j, \omega_1 - \omega_2) \\ &+ \Gamma_{ij}^*(\omega_1 - \omega_2) W_s(i - j, \omega_1 - \omega_2) \}. \end{aligned} \quad (42)$$

Substituting (39), (40), and (42) into (38) gives

$$\begin{aligned} \text{Cov} \{J_{sv}(\omega_1), J_{sv}(\omega_2)\} &= \left(\frac{P_r}{K_1 U_s T_G B_s}\right)^2 \\ &\cdot \sum_{i=1}^{K_1} \sum_{j=1}^{K_1} \left| \Gamma_{ij}(\omega_1 - \omega_2) \right. \\ &\left. + \frac{1}{\text{SNR}} W_s(i - j, \omega_1 - \omega_2) \right|^2, \\ &\text{for all } \omega_1, \omega_2 \in (\omega_l, \omega_h) \end{aligned} \quad (43)$$

where

$$\text{SNR} = \frac{P_r}{B_s b}. \quad (44)$$

Therefore, from (36) and (43) we see that

$$\begin{aligned} \text{Var} [C_1] &= E \left\{ \left( \sum_{k=k_l}^{k_h} J_{sv}(k) - E[J_{sv}(k)] \right)^2 \right\} \\ &= \sum_{k_1=k_l}^{k_h} \sum_{k_2=k_l}^{k_h} \text{Cov} \{J_{sv}(k_1), J_{sv}(k_2)\} \\ &= \frac{P_r^2}{(U_s K_1)^2 (T_G B_s)^2} \sum_{k_1=k_l}^{k_h} \sum_{k_2=k_l}^{k_h} \sum_{i=1}^{K_1} \sum_{j=1}^{K_1} \\ &\cdot \left| \Gamma_{ij}(k_1 - k_2) + \frac{1}{\text{SNR}} W_s(i - j, k_1 - k_2) \right|^2 \\ &= \frac{P_r^2}{(U_s K_1)^2 T_G B_s} \sum_{k=-k_s}^{k_s} \sum_{i=1}^{K_1} \sum_{j=1}^{K_1} \\ &\cdot \left| \Gamma_{ij}(k) + \frac{1}{\text{SNR}} W_s(i - j, k) \right|^2 \left(1 - \frac{|k|}{k_s}\right) \end{aligned} \quad (45)$$

where  $\Gamma_{ij}(k) = \Gamma_{ij}(\omega = 2\pi k/M)$  and  $W_s(i, k) = W_s(i, \omega = 2\pi k/M)$ .

### B. Mean and Variance of $C_2$

For the bottom path of Fig. 2, only noise is present. The mean and variance of  $C_2$  can be directly obtained from (37), (44), and (45) by letting  $P_r \rightarrow 0$ , and setting  $K_1 = K_2$ ,  $W_s(q, k) = W_N(q, k)$ ,  $M = N$  and  $B_s = B_N$ , i.e.

$$E[C_2] = k_v \left(\frac{b}{T}\right) = N \left(\frac{f'_h}{f'_s} - \frac{f'_l}{f'_s}\right) \left(\frac{b}{T}\right) = T_N B_N \left(\frac{b}{T}\right) \quad (46)$$

$$\begin{aligned} \text{Var} [C_2] &= \left(\frac{b}{U_N}\right)^2 \left(\frac{B_N}{T_N}\right) \frac{1}{K_2} \sum_{k=-k_s}^{k_s} \sum_{q=-K_2}^{K_2} |W_N(q, k)|^2 \\ &\cdot \left(1 - \frac{|q|}{K_2}\right) \left(1 - \frac{|k|}{k_v}\right) \end{aligned} \quad (47)$$

where

$$U_N = \frac{1}{N} \sum_{n=0}^{N-1} w_N^2(n). \quad (48)$$

$W_N(q, \omega)$  is the Fourier transform of

$$w_N(q, n) = w_N(n) w_N(n + qD_2). \quad (49)$$

$W_N(q, k) = W_N(q, \omega = 2\pi k/N)$ ,  $T_N = NT$ ,  $k_v = k'_h - k'_l + 1 \approx T_N B_N$ , and  $k'_l$  and  $k'_h$  are the smallest and largest integers in  $(f'_l NT, f'_h NT)$ .

### C. $K_p$ of an Unbiased Estimate of $P_r$

From (37) and (46) one can form an unbiased estimate for  $P_r$ , as

$$\hat{P}_r = \frac{U_s T}{U_s^* T_G} \left( C_1 - \frac{T_G B_s}{T_N B_N} C_2 \right). \quad (50)$$

Note that  $T_G = MT$  and  $T_N = NT$  denote the time interval of one data segment for the top and the bottom signal path in Fig. 2, respectively.

Finally, we have

$$\text{Var} [\hat{P}_r] = \left(\frac{U_s T}{U_s^* T_G}\right)^2 \left\{ \text{Var} (C_1) + \left(\frac{T_G B_s}{T_N B_N}\right)^2 \text{Var} (C_2) \right\}. \quad (51)$$

Combining (45), (47), and (51), and substituting into (12) leads to the expression for  $K_p$  as follows:

$$\begin{aligned} K_p &= \frac{1}{\sqrt{T_G B_s}} \left(\frac{1}{M U_s^*}\right) \left\{ \frac{1}{K_1^2} \left[ \sum_{k=-k_s}^{k_s} \sum_{i=1}^{K_1} \sum_{j=1}^{K_1} \right. \right. \\ &\cdot \left| \Gamma_{ij}(k) + \frac{1}{\text{SNR}} W_s(i - j, k) \right|^2 \left(1 - \frac{|k|}{k_s}\right) \\ &+ \frac{1}{K_2} \left(\frac{T_G B_s}{T_N B_N}\right) \left(\frac{M U_s}{N U_N}\right)^2 \frac{1}{\text{SNR}^2} \left[ \sum_{k=-k_s}^{k_s} \sum_{q=-K_2}^{K_2} \right. \\ &\cdot \left. \left. |W_N(q, k)|^2 \left(1 - \frac{|k|}{k_v}\right) \left(1 - \frac{|q|}{K_2}\right) \right] \right\}^{1/2}. \end{aligned} \quad (52)$$

The resulting  $K_p$  equation appears to be complicated. However, we will consider two particular examples in the next section. One of these examples shows that this expression reduces to the well-known analog  $K_p$  equation. The other example shows that this expression reduces to the normalized standard deviation of Welch's power spectrum estimate when  $k_s = 1$  and  $\text{SNR} = \infty$ .

#### IV. EXAMPLES OF EVALUATING THE DIGITAL $K_p$ EQUATION

The first example is for  $K_1 = K_2 = 1$ ,  $(T_G/T_s) \ll k_s < M/2$ ,  $w_s(n)$ , and  $w_N(n)$  are rectangular windows. This case should correspond to the analog filter processor. For this example,  $U_s = U_N = 1$ ,  $U_s^* = T_s/T_G$ ,  $W_s(0, 0) = M$ ,  $W_N(0, 0) = N$ ,  $\Gamma_{11}(0) = MT_s/T_G$ , and

$$\sum_{k=0}^{M-1} \frac{|\Gamma_{11}(k)|^2}{M^2} = \sum_{n=0}^{M-1} \frac{\gamma_{11}^2(n)}{M} = \frac{T_s}{T_G}$$

The  $K_p$  is then

$$\begin{aligned} K_p &= \frac{1}{\sqrt{T_G B_s}} \frac{T_G}{M T_s} \left\{ \sum_{k=0}^{M-1} |\Gamma_{11}(k)|^2 + \frac{1}{\text{SNR}^2} |W_s(0, 0)|^2 \right. \\ &\quad \left. + \frac{2}{\text{SNR}} \Gamma_{11}(0) W_s(0, 0) \right. \\ &\quad \left. + \left( \frac{T_G B_s}{T_N B_N} \right) \left( \frac{M}{N} \right)^2 \frac{1}{\text{SNR}^2} |W_N(0, 0)|^2 \right\}^{1/2} \\ &= \frac{1}{\sqrt{T_G B_s}} \frac{T_G}{M T_s} \left\{ M^2 \left( \frac{T_s}{T_G} \right) + \frac{M^2}{\text{SNR}^2} \right. \\ &\quad \left. + \frac{2}{\text{SNR}} M^2 \frac{T_s}{T_G} + \frac{1}{\text{SNR}^2} M^2 \frac{T_G B_s}{T_N B_N} \right\}^{1/2} \\ &= \frac{1}{\sqrt{T_s B_s}} \left\{ 1 + \frac{2}{\text{SNR}} + \frac{1}{\text{SNR}^2} \left( \frac{T_G}{T_s} \right) \left( 1 + \frac{T_G B_s}{T_N B_N} \right) \right\}^{1/2} \end{aligned} \quad (53)$$

Equation (53) is exactly the analog filter expression derived in [7] (also, see [3]). This example provides a connection of the  $K_p$  equations for analog and digital signal processors.

As a second example, we examine the  $K_p$  equation for  $T_G = T_s = T_N$ ,  $D_1 = D_2$ ,  $B_s = B_N$ ,  $K_1 = K_2 = K$ . Thus,  $M = N$  and  $U_s = U_N = U_s^*$  and  $\Gamma_{ij}(k) = W_s(i - j, k) = W_N(i - j, k)$ . Equation (52) then reduces to

$$\begin{aligned} K_p &= \frac{1}{\sqrt{k_s}} \frac{1}{M U_s} \frac{1}{\sqrt{K}} \left( 1 + \frac{2}{\text{SNR}} \pm \frac{2}{\text{SNR}^2} \right)^{1/2} \\ &\quad \cdot \left\{ \sum_{k=-k_s}^{k_s} \sum_{q=-K}^K |W_s(q, k)|^2 \right. \\ &\quad \left. \cdot \left( 1 - \frac{|k|}{k_s} \right) \left( 1 - \frac{|q|}{K} \right) \right\}^{1/2} \end{aligned} \quad (54)$$

We will discuss two special cases for this example.

*Case I.* Assume that  $k_s = 1$  and  $\text{SNR} = \infty$ . The resulting  $K_p$  should correspond to the normalized standard deviation of Welch's power spectrum estimate. First, let us consider the nonoverlapping case where  $W_s(q, k) = 0$  for  $q \neq 0$ . The  $K_p$  equation (54) can be further reduced to

$$\begin{aligned} K_p &= \frac{1}{M U_s} \frac{1}{\sqrt{K}} |W_s(0, 0)| \\ &= \frac{1}{M U_s} \frac{1}{\sqrt{K}} \left( \sum_{n=0}^{M-1} w_s^2(n) \right) = \frac{1}{\sqrt{K}} \end{aligned} \quad (55)$$

which was also shown by Welch [6].

Second, let us consider the 50-percent overlapping case ( $D = M/2$ ). In this case,  $W_s(q, k) = 0$  for  $q > 1$ . Equation (54) can be expressed as

$$\begin{aligned} K_p &= \frac{1}{M U_s} \frac{1}{\sqrt{K}} \left\{ |W_s(0, 0)|^2 + 2 \right. \\ &\quad \left. \cdot \left( 1 - \frac{1}{K} \right) |W_s(1, 0)|^2 \right\}^{1/2} \end{aligned} \quad (56)$$

Following an example in Welch's paper, we examine the case with the following window function:

$$\begin{aligned} w_s(n) &= 1 - \left( \frac{n - \frac{M-1}{2}}{\frac{M+1}{2}} \right)^2 \\ &0 \leq n \leq M-1. \end{aligned} \quad (57)$$

For this case

$$|W_s(1, 0)|^2 \cong \frac{1}{3} |W_s(0, 0)|^2.$$

Therefore

$$\begin{aligned} K_p &= \frac{1}{M U_s} \frac{1}{\sqrt{K}} \left( \frac{11}{9} - \frac{2}{9K} \right)^{1/2} |W_s(0, 0)| \\ &\cong \frac{1}{M U_s} \frac{1}{\sqrt{K}} \left( \frac{11}{9} \right)^{1/2} |W_s(0, 0)| = \left( \frac{11}{9} \right)^{1/2} \frac{1}{\sqrt{K}} \end{aligned} \quad (58)$$

which is the same as the results shown in [6]. As previously stated, Welch's power spectrum estimation results are special cases of the derived  $K_p$  equation.

*Case II.* Assume that  $w_s(n)$  is a generalized Hamming window given by

$$\begin{aligned} w_s(n) &= \alpha - (1 - \alpha) \cos \left( \frac{2\pi n}{M} \right), \\ &0 \leq n \leq M-1. \end{aligned} \quad (59)$$

Note that it is a rectangular window (i.e., no weight) for  $\alpha = 1$ , and a Hamming window for  $\alpha = 0.5$ .  $W_s(0, k)$  can be easily shown to be

$$W_s(0, k) = \begin{cases} (\alpha^2 + \frac{1}{2}(1 - \alpha)^2)M, & k = 0 \\ -\alpha(1 - \alpha)M, & k = 1, M-1 \\ \frac{1}{2}(1 - \alpha)^2 M, & k = 2, M-2 \\ 0, & \text{otherwise} \end{cases} \quad (60)$$

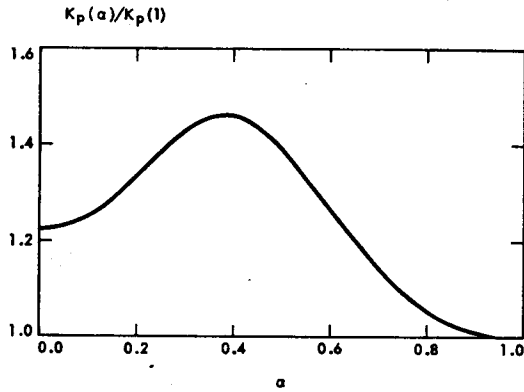


Fig. 3.  $K_p(\alpha)/K_p(1)$  for a generalized Hamming window for one data segment.

and  $U_s = W_s(0, 0)/M = \alpha^2 + \frac{1}{2}(1 - \alpha)^2$ . First, let us consider the case  $K = 1$  and  $2 \ll k_s < M/2$ . For this special case, (54) can be reduced to

$$\begin{aligned}
 K_p &= \frac{1}{\sqrt{k_s}} \frac{1}{MU_s} \left( 1 + \frac{2}{\text{SNR}} + \frac{2}{\text{SNR}^2} \right)^{1/2} \\
 &\quad \cdot \left\{ \sum_{k=0}^{M-1} |W_s(0, k)|^2 \right\}^{1/2} \\
 &= \frac{1}{\sqrt{k_s}} \frac{(\alpha^4 + 3\alpha^2(1 - \alpha)^2 + \frac{3}{8}(1 - \alpha)^4)^{1/2}}{\alpha^2 + \frac{1}{2}(1 - \alpha)^2} \\
 &\quad \cdot \left( 1 + \frac{2}{\text{SNR}} + \frac{2}{\text{SNR}^2} \right)^{1/2} \quad (61)
 \end{aligned}$$

The ratio of  $K_p(\alpha)$  to  $K_p(1)$  versus  $\alpha$  is plotted in Fig. 3. This verifies that, indeed, as mentioned in the introduction, the use of windows increases  $K_p$  and therefore degrades system performance.

Next, we consider the overlapping case with  $\text{SNR} = 1$ ,  $M = 256$ , and  $L = 1024$ . We directly compute  $K_p$  using (54) for  $K = 4$  with nonoverlapping,  $K = 5$  with 25-percent overlapping,  $K = 7$  with 50-percent overlapping,  $K = 13$  with 75-percent overlapping data segment, and  $K = 25$  with 87.5-percent overlapping data segment. The resulting  $K_p$ 's (as function of  $\alpha$ ) are shown in Fig. 4(a)-(d) for  $k_s = 1, 2, 4$ , and  $64$ , respectively. Note that the  $\sigma_0$  cells associated with  $k_s = 1, 2$ , and  $4$  are much smaller than the  $\sigma_0$  cell associated with  $k_s = 64$  because  $B_s = k_s f_s / M$ . From Fig. 4(a) we see that  $K_p$  does not depend on the window for the nonoverlapping case when  $k_s = 1$ . Data segment overlapping improves  $K_p$ . The amount of improvement depends on the window chosen. Notice that when  $k_s = 1$  the correlation between frequency bins due to windowing and data segment overlapping does not appear in the  $K_p$  equation. When  $k_s > 1$ , the correlation between frequency bins due to windowing and data seg-

ment overlapping may actually degrade  $K_p$  (see Fig. 4(b)-(d)).

Finally, we consider  $K_p$  versus the percentage in data segment overlap for  $\text{SNR} = 1$ ,  $M = 256$ ,  $L = 8192$ ,  $k_s = 4$ , and  $\alpha = 0.5$  (Hamming window). The result is shown in Fig. 5. From this figure we see that  $K_p$  decreases as the amount of overlap increases and approaches an asymptote for overlap greater than 50 percent. In other words, little improvement in  $K_p$  is obtained when the amount of overlapping is more than 50 percent.

We note that a generalized Hamming window is very narrow in the frequency domain because only three values are nonzero for  $0 \leq k \leq M - 1$ . The hardware required to implement the generalized Hamming window can be quite simple because it only involves three frequency bins for convolution in the frequency domain.

## V. DISCUSSION

A digital Doppler processor is planned for on-board digital signal processing for NSCAT. In this paper, we have derived an expression for the normalized standard deviation of backscatter power measurements  $K_p$  for such a digital signal processor. The effects of two digital signal processing techniques, namely windowing and data segment overlap processing, are treated. Windowing must be invoked in cases where spectral leakage is to be minimized in order to avoid inter- $\sigma_0$  cell interference. When windowing is used, overlap processing may then be considered to minimize the system performance degradation due to the windowing. Although the resulting expression for  $K_p$  is quite complex, we have demonstrated that it reduces to the well-known  $K_p$  expression for analog signal processors and that Welch's power spectrum estimation results [6] are special cases of the derived  $K_p$  expression.

In the NSCAT baseline design, a Hamming window and 50-percent overlap processing will be used. The Hanning window, applied through convolution in frequency domain, was chosen because it minimizes spectral leakage and is simple to implement. In fact, since the window weights are  $\frac{1}{2}$  and  $\frac{1}{4}$ , only bit shifting, addition and subtraction are required without any multiplication. This lessens the computation load in a spaceborne processor. Based on  $K_p$  values versus computational load, a 50-percent overlap was chosen for the baseline design (see Fig. 5). There are on-going efforts to refine this baseline design using the  $K_p$  expression.

In addition to utilizing a digital signal processor to improve system performance, NSCAT also plans to use six antennas in contrast to the four antennas on SASS. Each side of the subsatellite track will be illuminated by three antennas. They will provide three different azimuthal observations of  $\sigma_0$  from the ocean for wind vector estimation. This will simplify data interpretation by reducing the number of ambiguities in the estimated wind direction (see [3] and [9]).

Details of the NSCAT design, as well as further trade-offs in the digital Doppler processors will be reported in future papers.

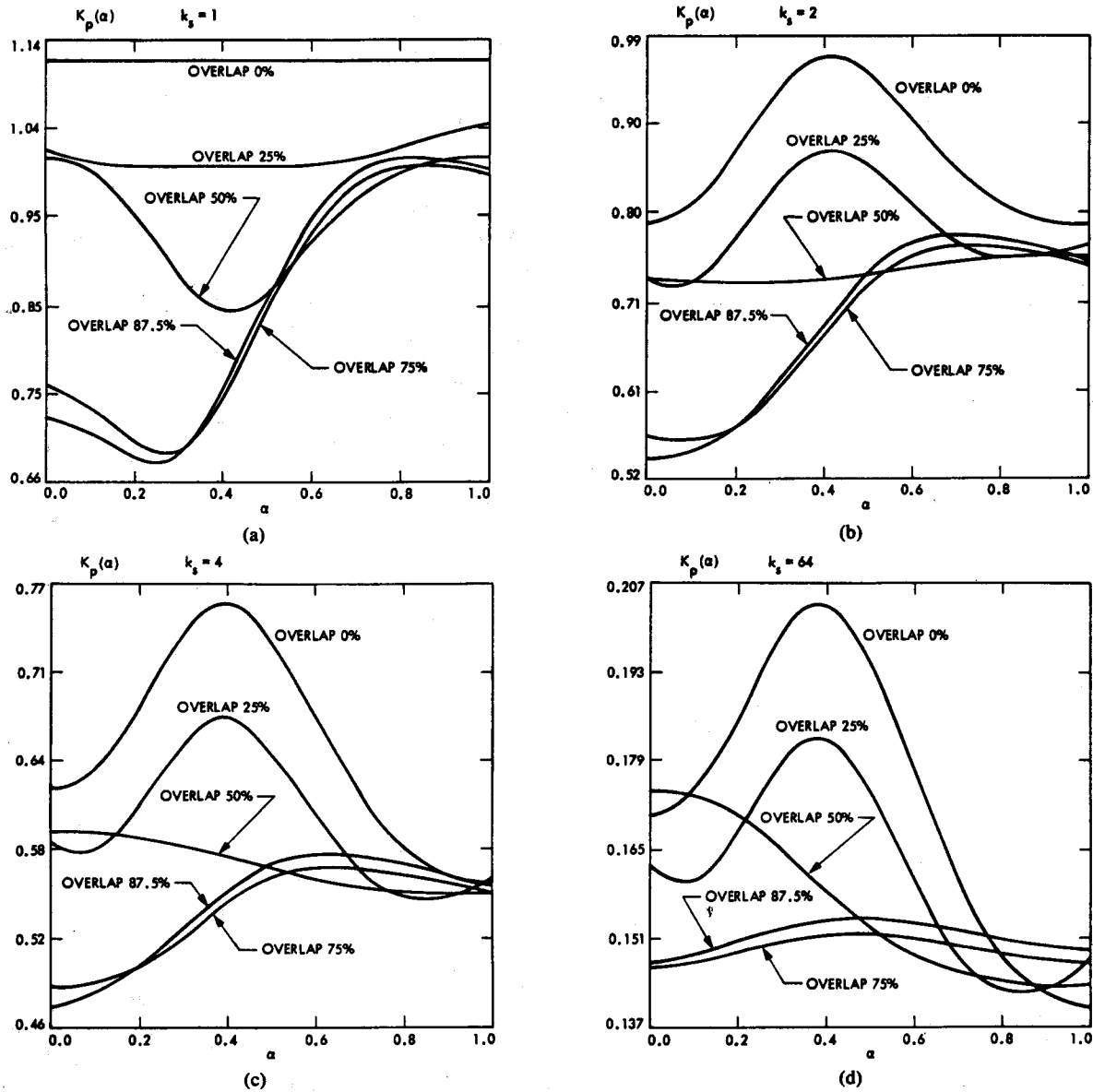


Fig. 4:  $K_p(\alpha)$  for a generalized Hamming window and overlapping and nonoverlapping segments for (a)  $k_s = 1$ , (b)  $k_s = 2$ , (c)  $k_s = 4$ , and (d)  $k_s = 64$ , respectively.

APPENDIX I

PROOF OF EQUATION (11)

From (4) we have

$$\begin{aligned}
 & E\{J_i(\omega_1) J_r(\omega_2)\} \\
 &= \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \\
 &\cdot E \left\{ \sum_k \sum_l \sum_m \sum_n x_i(k) x_i(l) x_r(m) x_r(n) \right. \\
 &\cdot \gamma_i(k) \gamma_i(l) \gamma_r(m) \gamma_r(n) \\
 &\cdot \left. \exp(j[\omega_1(k-l) + \omega_2(m-n)]) \right\}. \quad (A1)
 \end{aligned}$$

For a zero-mean stationary Gaussian process  $x(n)$ , it is well known that

$$\begin{aligned}
 & E[x_i(k) x_i(l) x_r(m) x_r(n)] \\
 &= E[x_i(k) x_i(l)] E[x_r(m) x_r(n)] \\
 &\quad + E[x_i(k) x_r(m)] E[x_i(l) x_r(n)] \\
 &\quad + E[x_i(k) x_r(n)] E[x_i(l) x_r(m)] \\
 &= \phi_x(l-k) \phi_x(n-m) \\
 &\quad + \phi_x(k-m+qD) \phi_x(l-n+qD) \\
 &\quad + \phi_x(k-n+qD) \phi_x(l-m+qD) \quad (A2)
 \end{aligned}$$

where  $\phi_x(k)$  is the correlation function of  $x(n)$ , and

$$q = i - r. \quad (A3)$$

Thus

$$E\{J_i(\omega_1) J_r(\omega_2)\} = Q_1 + Q_2 + Q_3 \quad (A4)$$



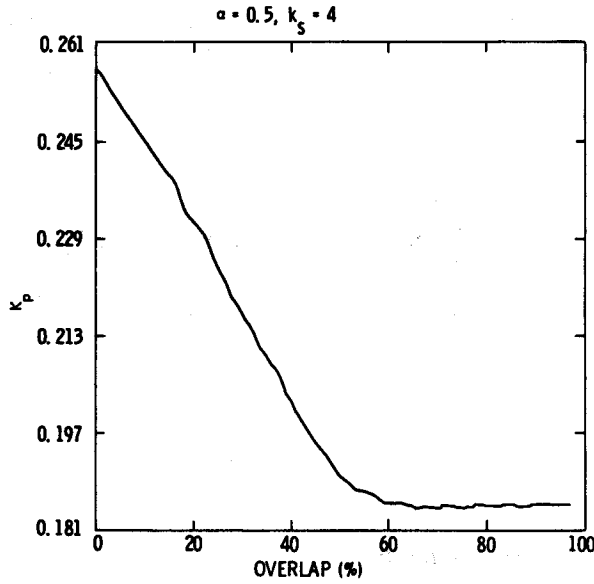


Fig. 5.  $K_p$  versus overlapping for  $k_s = 4$  and  $\alpha = 0.5$ .

where

$$Q_1 = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \left\{ \sum_k \sum_l \sum_m \sum_n \right. \\ \cdot \phi_x(l-k) \phi_x(n-m) \gamma_i(k) \gamma_i(l) \gamma_r(m) \gamma_r(n) \\ \cdot \exp [j[\omega_1(k-l) + \omega_2(m-n)]] \left. \right\} \quad (A5)$$

$$Q_2 = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \sum_k \sum_l \sum_m \sum_n \\ \cdot \{ \phi_x(k-m+qD) \\ \cdot \phi_x(l-n+qD) \gamma_i(k) \gamma_i(l) \gamma_r(m) \gamma_r(n) \\ \cdot \exp [j[\omega_1(k-l) + \omega_2(m-n)]] \} \quad (A6)$$

and

$$Q_3 = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \sum_k \sum_l \sum_m \sum_n \\ \cdot \{ \phi_x(k-n+qD) \phi_x(l-m+qD) \\ \cdot \gamma_i(k) \gamma_i(l) \gamma_r(m) \gamma_r(n) \\ \cdot \exp [j[\omega_1(k-l) + \omega_2(m-n)]] \}. \quad (A7)$$

We now derive  $Q_1$ ,  $Q_2$ , and  $Q_3$ . Because the power density spectrum  $P_x(\omega)$  of  $x(n)$  is the Fourier transform of  $\phi_x(n)$ ,  $Q_1$  can be expressed in frequency domain

$$Q_1 = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \sum_k \sum_l \sum_m \sum_n \\ \cdot \left\{ \left(\frac{1}{2\pi}\right)^2 \int_{-\pi}^{\pi} P_x(\theta_1) \exp [j\theta_1(l-k)] d\theta_1 \right. \\ \cdot \left. \int_{-\pi}^{\pi} P_x(\theta_2) \exp [j\theta_2(n-m)] \right.$$

$$\cdot d\theta_2 \gamma_i(k) \gamma_i(l) \gamma_r(m) \gamma_r(n) \\ \cdot \left. \exp [j[\omega_1(k-l) + \omega_2(m-n)]] \right\} \\ = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \left\{ \left(\frac{1}{2\pi}\right)^2 \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} P_x(\theta_1) P_x(\theta_2) \right. \\ \cdot \sum_k \sum_l \sum_m \sum_n \gamma_i(k) \gamma_i(l) \gamma_r(m) \gamma_r(n) \\ \cdot \exp [-j(\omega_1 - \theta_1)(l-k)] \\ \cdot \exp [-j(\omega_2 - \theta_2)(n-m)] d\theta_1 d\theta_2 \left. \right\} \\ = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \left(\frac{1}{2\pi}\right)^2 \\ \cdot \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} P_x(\theta_1) P_x(\theta_2) |\Gamma_r(\omega_1 - \theta_1)|^2 \\ \cdot |\Gamma_r(\omega_2 - \theta_2)|^2 d\theta_1 d\theta_2 \\ = E[J_r(\omega_1)] E[J_r(\omega_2)]. \quad (A8)$$

Therefore

$$\text{Cov} \{J_i(\omega_1), J_r(\omega_2)\} = Q_2 + Q_3. \quad (A9)$$

From (A6) we have

$$Q_2 = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \left(\frac{1}{2\pi}\right)^2 \\ \cdot \left\{ \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} P_x(\theta_1) P_x(\theta_2) \sum_k \sum_l \sum_m \sum_n \right. \\ \cdot \gamma_i(k) \gamma_i(l) \gamma_r(m) \gamma_r(n) \cdot \exp [j[\theta_1(k-m) \\ + \theta_2(l-n) + \omega_1(k-l) + \omega_2(m-n)]] \\ \cdot \exp [j(\theta_1 + \theta_2) qD] d\theta_1 d\theta_2 \left. \right\} \\ = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \left(\frac{1}{2\pi}\right)^2 \left\{ \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} P_x(\theta_1) P_x(\theta_2) \right. \\ \cdot \Gamma_i^*(\theta_1 + \omega_1) \Gamma_i^*(\theta_2 - \omega_1) \Gamma_r(\theta_1 - \omega_2) \\ \cdot \Gamma_r(\theta_2 + \omega_2) \cdot \exp [j(\theta_1 + \theta_2) qD] d\theta_1 d\theta_2 \left. \right\} \\ = \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \left(\frac{1}{2\pi}\right)^2 \left\{ \int_{-\pi}^{\pi} P_x(\theta_1) \Gamma_i^*(\theta_1 + \omega_1) \right. \\ \cdot \Gamma_r(\theta_1 - \omega_2) \exp [j\theta_1 qD] d\theta_1 \left. \right\} \\ \cdot \left\{ \int_{-\pi}^{\pi} P_x(\theta_2) \Gamma_i^*(\theta_2 - \omega_1) \Gamma_r(\theta_2 + \omega_2) \right. \\ \cdot \exp [j\theta_2 qD] d\theta_2 \left. \right\}.$$

$$\begin{aligned}
&\equiv \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_j}\right) P^2 \left\{ \frac{1}{2\pi} \int_{-\pi}^{\pi} \Gamma_i^*(\theta_1 + \omega_1) \right. \\
&\quad \cdot \Gamma_r(\theta_1 - \omega_2) \exp [j\theta_1 q D] d\theta_1 \left. \right\} \\
&\quad \cdot \left\{ \frac{1}{2\pi} \int_{-\pi}^{\pi} \Gamma_i^*(\theta_2 - \omega_1) \Gamma_r(\theta_2 + \omega_2) \right. \\
&\quad \cdot \exp [j\theta_2 q D] d\theta_2 \left. \right\} \\
&= \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_j}\right) P^2 |\Gamma_{ir}(\omega_1 + \omega_2)|^2, \\
&\quad \text{(since (B1)) for } \omega_1, \omega_2 \in (\omega_a, \omega_b). \quad (A10)
\end{aligned}$$

Similarly, we can show

$$\begin{aligned}
Q_3 &\equiv \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) \left(\frac{1}{2\pi}\right)^2 P^2 \left\{ \int_{-\pi}^{\pi} \Gamma_i^*(\theta_1 + \omega_1) \right. \\
&\quad \cdot \Gamma_r(\theta_1 + \omega_2) \exp [j\theta_1 q D] d\theta_1 \left. \right\} \\
&\quad \cdot \left\{ \int_{-\pi}^{\pi} \Gamma_i^*(\theta_2 - \omega_1) \Gamma_r(\theta_2 - \omega_2) \exp [j\theta_2 q D] d\theta_2 \right\} \\
&= \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) P^2 |\Gamma_{ir}(\omega_1 - \omega_2)|^2, \\
&\quad \text{for } \omega_1, \omega_2 \in (\omega_a, \omega_b). \quad (A11)
\end{aligned}$$

Thus

$$\begin{aligned}
&\text{Cov} \{J_i(\omega_1), J_r(\omega)\} \\
&= \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) P^2 \\
&\quad \cdot \{|\Gamma_{ir}(\omega_1 + \omega_2)|^2 + |\Gamma_{ir}(\omega_1 - \omega_2)|^2\} \\
&\equiv \left(\frac{1}{MU_i}\right) \left(\frac{1}{MU_r}\right) P^2 |\Gamma_{ir}(\omega_1 - \omega_2)|^2. \quad (A12)
\end{aligned}$$

Therefore

$$\begin{aligned}
\text{Cov} \{J(\omega_1), J(\omega_2)\} &\equiv \frac{1}{K^2} \left(\frac{P^2}{M^2}\right) \sum_{i=1}^K \sum_{j=1}^K \\
&\quad \cdot \left[ \frac{1}{U_i} \frac{1}{U_j} |\Gamma_{ij}(\omega_1 - \omega_2)|^2 \right]. \quad (A13)
\end{aligned}$$

### APPENDIX II AN INTEGRAL EQUATION

In this appendix, we prove the following identity equation:

$$\begin{aligned}
&\frac{1}{2\pi} \int_{-\pi}^{\pi} \Gamma_i^*(\theta - \omega_1) \Gamma_r(\theta + \omega_2) \exp [j\theta q D] d\theta \\
&= \Gamma_{ir}(\omega_1 + \omega_2) \exp [-j\omega_2 q D] \quad (B1)
\end{aligned}$$

where  $\Gamma_i(\omega)$ ,  $\Gamma_{ir}(\omega)$ , and  $\Gamma_r(\omega)$  are the Fourier transforms of  $\gamma_i(n)$ ,  $\gamma_r(n)$ , and  $\gamma_{ir}(n)$  (see (7)), respectively, and  $q = i - r$ .

*Proof:*

$$\begin{aligned}
&\frac{1}{2\pi} \int_{-\pi}^{\pi} \Gamma_i^*(\theta - \omega_1) \Gamma_r(\theta + \omega_2) \exp [j\theta q D] d\theta \\
&= \frac{1}{2\pi} \int_{-\pi}^{\pi} \Gamma_i(\omega_1 - \theta) \Gamma_r(\theta + \omega_2) \exp [j\theta q D] d\theta \\
&= \frac{1}{2\pi} \int_{-\pi}^{\pi} \Gamma_i(\omega_1 + \omega_2 - y) \Gamma_r(y) \\
&\quad \cdot \exp [j(y - \omega_2) q D] dy \\
&= \frac{1}{2\pi} \left\{ \int_{-\pi}^{\pi} \Gamma_i(\omega_1 + \omega_2 - y) \Gamma_r(y) \right. \\
&\quad \cdot \exp [jy q D] dy \left. \right\} \exp [-j\omega_2 q D] \\
&= \Gamma_i(\omega) * (\Gamma_r(\omega) \exp [j\omega q D])|_{\omega=\omega_1+\omega_2} \exp [-j\omega_2 q D] \\
&= \Gamma_{ir}(\omega_1 + \omega_2) \exp [-j\omega_2 q D].
\end{aligned}$$

### APPENDIX III PROOF OF EQUATION (42)

*Proof:* From (33) we have

$$\begin{aligned}
&\text{Cov} \{I_{sr}(\omega_1), I_{sr}(\omega_2)\} \\
&= \left(\frac{1}{MU_s K_1}\right)^2 \sum_{i=1}^{K_1} \sum_{r=1}^{K_1} 2 \text{Re} \{E[X_{s_i}(\omega_1) X_{s_r}(\omega_2)] \\
&\quad \cdot E[X_{s_i}^*(\omega_1) X_{s_r}^*(\omega_2)] + E[X_{s_i}(\omega_1) X_{s_r}^*(\omega_2)] \\
&\quad \cdot E[X_{s_r}(\omega_1) X_{s_i}(\omega_2)]\}. \quad (C1)
\end{aligned}$$

To further simplify (C1), we need to derive  $E[X_{s_i}(\omega_1) X_{s_r}^*(\omega_2)]$  as follows:

$$\begin{aligned}
E[X_{s_i}(\omega_1) X_{s_r}^*(\omega_2)] &= E \left\{ \sum_{m=0}^{M-1} \sum_{n=0}^{M-1} s(n + (i-1)D_1) \right. \\
&\quad \cdot \gamma_i(n) s(m + (r-1)D_1) \gamma_r(m) \\
&\quad \cdot \exp [-j(\omega_1 n - \omega_2 m)] \left. \right\} \\
&= \sum_{m=0}^{M-1} \sum_{n=0}^{M-1} \phi_s(n - m + (i-r)D_1) \\
&\quad \cdot \gamma_i(n) \gamma_r(m) \exp [-j(\omega_2 n - \omega_2 m)] \\
&= \sum_{m=0}^{M-1} \sum_{n=0}^{M-1} \left(\frac{1}{2\pi}\right) \int_{-\pi}^{\pi} P_s(\theta) \\
&\quad \cdot \exp [j(n - m + (i-r)D_1)\theta] \\
&\quad \cdot \exp [-j(\omega_1 n - \omega_2 m)] \gamma_i(n) \gamma_r(m) d\theta
\end{aligned}$$

$$\begin{aligned}
E[X_{si}(\omega_1) X_{sj}^*(\omega_2)] &= \frac{1}{2\pi} \int_{-\pi}^{\pi} P_s(\theta) \Gamma_i^*(\theta - \omega_1) \\
&\quad \cdot \Gamma_r(\theta - \omega_2) \exp [j(i - r)D_1\theta] d\theta \\
&= \frac{P_r}{B_s T} \left( \frac{1}{2\pi} \right) \int_{-\pi}^{\pi} \Gamma_i^*(\theta - \omega_1) \\
&\quad \cdot \Gamma_r(\theta - \omega_2) \exp [j(i - r)D_1\theta] d\theta \\
&= \frac{P_r}{B_s T} \Gamma_{ir}(\omega_1 - \omega_2) \exp [j\omega_2(i - r)D_1], \\
&\quad \text{(from (B1)) for } \omega_1, \omega_2 \in (\omega_l, \omega_h).
\end{aligned} \tag{C2}$$

Similarly, one can easily show that

$$\begin{aligned}
E[X_{sr}(\omega_1) X_{ss}(\omega_2)] &= \frac{P_r}{B_s T} \Gamma_{ir}(\omega_1 + \omega_2) \\
&\quad \cdot \exp [-j\omega_2(i - r)D_1] \\
&\quad \omega_1, \omega_2 \in (\omega_l, \omega_h)
\end{aligned} \tag{C3}$$

$$\begin{aligned}
E[X_{vr}^*(\omega_1) X_{vs}^*(\omega_2)] &= \left( \frac{b}{T} \right) W_s^*(i - r, \omega_1 + \omega_2) \\
&\quad \cdot \exp [j\omega_2(i - r)D_1] \\
&\quad \omega_1, \omega_2 \in (\omega_l, \omega_h),
\end{aligned} \tag{C4}$$

and

$$\begin{aligned}
E[X_{vr}^*(\omega_1) X_{vs}(\omega_2)] &= \left( \frac{b}{T} \right) W_s^*(i - r, \omega_1 - \omega_2) \\
&\quad \cdot \exp [-j\omega_2(i - r)D_1] \\
&\quad \omega_1, \omega_2 \in (\omega_l, \omega_h).
\end{aligned} \tag{C5}$$

Substituting (C2) through (C5) into (C1) gives

$$\begin{aligned}
\text{Cov} \{I_{sv}(\omega_1), I_{sv}(\omega_2)\} \\
&= 2 \left( \frac{P_r}{B_s} \right) b \left( \frac{1}{T_G U_s K_1} \right)^2 \\
&\quad \cdot \sum_{i=1}^{K_1} \sum_{r=1}^{K_1} \text{Re} \{ \Gamma_{ir}(\omega_1 - \omega_2) W_s^*(i - r, \omega_1 - \omega_2) \\
&\quad + \Gamma_{ir}(\omega_1 + \omega_2) W_s^*(i - r, \omega_1 + \omega_2) \} \\
&\equiv 2 \left( \frac{P_r}{B_s} \right) b \left( \frac{1}{T_G U_s K_1} \right)^2 \sum_{i=1}^{K_1} \sum_{r=1}^{K_1} \\
&\quad \cdot \text{Re} \{ \Gamma_{ir}(\omega_1 - \omega_2) W_s^*(i - r, \omega_1 - \omega_2) \}
\end{aligned} \tag{C6}$$

which implies (42).

#### REFERENCES

- [1] R. K. Moore and F. T. Ulaby, "The radar radiometer," *Proc. IEEE*, vol. 57, pp. 587-590, Apr. 1969.
- [2] W. L. Jones, L. C. Schroeder, D. H. Boggs, E. M. Bracalente, R. A. Brown, G. J. Dome, W. J. Pierson, and F. J. Wentz, "The Seasat-A satellite scatterometer: The geophysical evaluation of re-

motely sensed wind vectors over the ocean," *J. Geophys. Res.*, vol. 87, no. C5, pp. 3297-3317, 1982.

- [3] E. Bracalente, E. D. Boggs, W. Grantham, and J. Sweet, "The SASS scattering coefficient ( $\sigma_0$ ) algorithm," *IEEE J. Ocean. Eng.*, vol. OE-5, Apr. 1980.
- [4] F. Li, P. Callahan, D. Lame, and C. Winn, "NASA scatterometer on NROSS—A system for global observations of oceanic winds," *Proc. IGARSS '84* (Strasbourg, France), Aug. 1984.
- [5] D. Long, C. Y. Chi, and F. Li, "Digital filter processor design for spaceborne scatterometers," *Proc. of IGARSS '84* (Strasbourg, France), Aug. 1984.
- [6] P. Welch, "The use of fast Fourier transform for the estimation of power spectra: A method based on time averaging over short, modified periodograms," *IEEE Trans. Audio Electroacoust.*, vol. AU-15, pp. 70-73, June 1967.
- [7] R. Fisher, "Standard deviation of scatterometer measurements from space," *IEEE Trans. Geosci. Electron.*, vol. GE-10, no. 2, pp. 106-113, Apr. 1972.
- [8] A. Oppenheim and R. Schaffer, *Digital Signal Processing*. Englewood Cliffs, NJ: Prentice-Hall, 1975.
- [9] L. C. Schroeder, W. L. Grantham, E. M. Bracalente, C. L. Britt, K. S. Shanmugan, F. J. Wentz, D. F. Wylie, and B. B. Hinton, "Removal of ambiguous wind directions for a Ku-band scatterometer using three different azimuth angles," *IEEE Trans. Geosci. Remote Sensing*, vol. GE-23, no. 2, pp. 91-100, Mar. 1985.
- [10] L. C. Schroeder, D. H. Boggs, G. Dome, I. M. Halbertam, W. L. Jones, W. J. Pierson, and F. J. Wentz, "The relationship between wind vector and normalized radar cross section used to derive SEASAT-A satellite scatterometer winds," *J. Geophys. Res.*, vol. 87, no. C5, pp. 3318-3336, Apr. 1982.



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